



International
Conference
EWaS

27-30 June 2018

Hotel Ionian Blue
Lefkada Island, Greece

3rd EWaS (Efficient Water Systems) International Conference:
insights on the **W**ater-**E**nergy-**F**ood Nexus



Second Announcement and Call for Papers

The 3rd EWaS International Conference is organized by the University of Thessaly, Civil Engineering Department. The conference focuses on efficient water systems giving insights on the Water-Food-Energy Nexus. Scientists will address and discuss issues related to hydraulics, hydrology, water resources systems management, climate change and environmental systems. Special emphasis will be given to the latest developments, strategies, techniques and applications in urban water and wastewater management, environmental protection and the interaction among Water, Energy and Food. International case studies will be presented to bring together theory and practice.

THEMES AND TOPICS

- Theme A: HYDRAULICS
- Theme B: URBAN WATER MANAGEMENT
- Theme C: WATER - ENERGY - FOOD NEXUS
- Theme D: RIVERINE SYSTEMS
- Theme E: HYDRODYNAMICS AND WAVES
- Theme F: GLOBAL CHANGES AND SMART CITIES
- Theme G: HYDROLOGY
- Theme H: RAW & WASTE WATER TREATMENT - WASTE MANAGEMENT
- Theme I: GROUNDWATER AND IRRIGATION SYSTEMS
- Theme J: ADVANCED METHODS FOR ENVIRONMENTAL SYSTEM ANALYSIS

Special Sessions

- SS1: "Small-scale hydropower generation in urban and rural areas: the hydraulic and mechanical analysis of Energy Recovery in water systems" (chair: prof. Maurizio Giugni)
- SS2: "Water distribution system modeling, simulation and management" (chair: prof. Marco Franchini)
- SS3: "Advances in Risk and Uncertainty Analysis of Hydrological and Water Resources Systems" (chair: prof. Athanasios Loukas)
- SS4: "Waterborne Diseases" (chair: prof. Dr. Panagiotis Karanis)
- SS5: "Groundwater Simulation and Optimization" (chair: prof. George P. Karatzas)
- SS6: "Water4Cities - Holistic Surface Water and Groundwater Management for Sustainable Cities" (chair: assoc. prof. Chrysi Laspidou)

Parallel Session

During the 3rd EWaS International Conference, one parallel technical workshop will take place at the context of the project «WATenERgy CYCLE - Urban water full cycle: from its source to its end-users and back to the environment».

Invited Speakers

Prof. **Jacques Ganoulis**, Special Secretary for Water and Director of the UNESCO Chair International Network of Water-Environment Centres for the Balkans
Prof. **George Tsakiris**, National Technical University of Athens, Greece and President of EWRA

Organized by the



UNIVERSITY of THESSALY
CIVIL ENGINEERING DEPARTMENT

ANALYSIS IMPORTANT DATES (extended)

Submission of abstracts: November 20th, 2017
Notification of acceptance: December 10th, 2017
Submission of full paper: January 31st, 2018
Early Bird Registration: January 31st, 2018

REGISTRATION FEES

(* money transfer/bank commission charges not included)

	Early Bird (till 31/1/2018)	Late Bird (till 31/3/2018)	After 31/3/2018 & On site
Standard Fee *	320€	400€	480€
Student's Fee **	150€	180€	200€
1-Day participation fee (applies only to those attending the conference and not to the authors)	120€	130€	150€
Accompanying Persons fee ***	100€	100€	100€

Please note: To submit a full paper (oral or poster) a registration fee must be paid first, until 31st of March 2018. In case a second paper by the same presenting author is submitted, an extra fee of 80€ is applicable. Also for the third paper (maximum submission for the same author) an extra fee of 80€ is applicable.

* Full Registration fee includes admittance at the welcome/ice-breaker reception, all five coffee breaks, one lunch, the official Gala dinner, and the boat trip around Lefkada Island and the main sightseeing points nearby. It also includes the Conference E-Proceedings.

** Student's fee includes admittance at the welcome/ice-breaker reception, all five coffee breaks, one lunch. It also includes the Conference E-Proceedings.

*** Accompanying Persons fees include admittance at the welcome/ice-breaker reception, the official Gala dinner, and the boat trip around Lefkada Island and the main sightseeing points nearby.

PUBLICATIONS

E-Proceedings with the full papers will be distributed at the Conference.

All papers presented at the Conference (either as oral presentations or as posters) will be eligible for publication in SCI journals with an Impact Factor supporting EWAS3, after being revised by at least 50% and following a standard peer-review process. The finally accepted papers will be published in either special or regular issues of the following Journals:

- Environmental Science and Pollution Research, Springer
- Journal of Hydroinformatics, IWA Publishing
- Water Science and Technology: Water Supply, IWA Publishing
- Water Science and Technology, IWA Publishing
- Desalination and Water Treatment, Desalination Publications
- Journal of Porous Media, Begell House
- Special Topics & Reviews in Porous Media: An International Journal, Begell House
- Environmental Processes, Springer
- Journal of Water Supply: Research and Technology - AQUA, IWA Publishing

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Venue

The Conference will be held at the 5-star hotel "Ionian Blue"

(<https://www.ionianblue.gr/start>) in Lefkada island.

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Conference Program

Venue: IONIAN BLUE HOTEL, Nikiana, Lefkada Island, Greece

27-30 JUNE 2018



“Insights on the **W**ater-**E**nergy-**F**ood Nexus”

REGISTRATION DESK IS OPEN:

Wednesday, June 27th: 09:30 – 13:00 & 16:00 – 20:00
Thursday, June 28th: 08:30 – 14:00 & 16:00 – 20:00
Friday, June 29th: 16:00 – 20:00
Saturday, June 30th: 10:00 – 13:00

WEDNESDAY, JUNE 27TH, 2018

09:30-13:00

Welcome of Participants

ROOM A

ROOM B

10:00-13:00

«WATenERgy CYCLE - Urban water full cycle: from its source to its end-users and back to the environment»

Workshop “Urban water - energy cycle efficiency: impacts on pricing policy”



10:00-13:00

FREEWAT Short Course



13:00-13:30

COFFEE BREAK

POSTER PRESENTATIONS

POSTER GROUP A THURSDAY, JUNE 28th (Presentation Period: 10:00-14:00)		POSTER GROUP B THURSDAY, JUNE 28th (Presentation Period: 16:00-20:00)	
EwaS3 081	TURBULENT SIMULATION OF THE FLOW AROUND DIFFERENT POSITIONS OF MUSSEL SHOCKS George Pechlivanidis, Evangelos Keramaris, Yiannis Savvidis	EwaS3 046	TREATMENT OF LANDFILL LEACHATE USING ULTRASOUND ASSISTED SBR REACTOR Anna Grosser, Ewa Neczaj, Magdalena Madela, Piotr Celary
EwaS3 082	MODELLING OF ENVIRONMENTAL PARAMETERS OF A HARBOR BASIN FORMED IN A COASTAL ZONE WITH A SEAWALL Yiannis Savvidis, Evangelos Keramaris, George Pechlivanidis, Christopher Koutitas	EwaS3 010	NUMERICAL MODELLING OF SOIL EROSION ON CEPHALONIA ISLAND GREECE USING GEOGRAPHICAL INFORMATION SYSTEMS AND THE REVISED SOIL LOSS EQUATION (RUSLE) Michail Xanthakis, Panagiotis Minetos, Georgia Lisitsa, Georgia Kamari
EwaS3 012	PERFORMANCE ANALYSIS OF BIOGAS FUELED SOFC HYBRID POWER SYSTEM Sunhee Kim, Kyung Chun Kim	EwaS3 065	ZERO-COST AGRICULTURAL WASTES AS SOURCES FOR ACTIVATED CARBONS SYNTHESIS: LEAD IONS REMOVAL FROM WASTEWATERS George Kyzas, Athanasios Mitropoulos
EwaS3 095	OPTIMUM SELECTION OF RENEWEABLE ENERGY POWERED DESALINATION SYSTEMS Ahmad Al-Jabr, Rached Ben-Mansour	EwaS3 061	OPTIMIZING SLUDGE MANAGEMENT AT THE MUNICIPAL SOLID WASTE INCINERATOR-A CASE STUDY Jakub Raček, Natalia Anferová, Petr Hlušík, Petr Hlavínek
EwaS3 023	INVESTIGATION OF THE RELATIONSHIP BETWEEN THREE- AND ONE-DIMENSIONAL INFILTRATION USING A MINI DISC INFILTRMETER George Kargas, Paraskevi Londra, Konstantinos Anastasiou	EwaS3 077	CLOSE RANGE PHOTOGRAMMETRY AND THERMAL IMAGERY IN MONITORING OF SOIL MOISTURE IN DAM STRUCTURES OF HISTORICAL FISHPONDS Josef Krása, Vaclav David
EwaS3 076	GEOPHYSICAL EVALUATION OF THE INNER STRUCTURE OF THE HISTORICAL EARTH-FILLED DAM David Zumr, Vaclav David, Josef Krasa, Jiří Nedvěď	EwaS3 056	INTEGRATED WATER RESOURCES MANAGEMENT IN THE MEDITERRANEAN: THE BONIS RIVER BASIN Giovanni Ravazzani, Tommaso Caloiero, Mouna Feki and Gaetano Pellicone
EwaS3 101	THE TESTING OF A SPRAYED BENTONITE SEALING LAYER Jiří Štástka, Vaclav David	EwaS3 075	ANALYSIS OF FLOOD HYDROGRAPHS IN OREDR TO PREDICT THE SHAPE OF THEIR FALLING LIMBS Vaclav David, Tereza Davidová
EwaS3 111	CIRCULAR ECONOMY IN WASTEWATER TREATMENT PLANT-CHALLENGES AND BARRIERS Ewa Neczaj, Anna Grosser	EwaS3 060	INVESTIGATION OF WATER CONSUMPTION VARIABILITY AT LOCAL SCALE IN PUGLIA (SOUTHERN ITALY) Gabriella Balacco, Antonio Carbonara, Andrea Gioia, Vito Iacobellis, Alberto Ferruccio Piccinni

Zero-cost agricultural wastes as sources for activated carbons synthesis: lead ions removal from wastewaters

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Abstract: In the present study, activated carbons (PAC) were hydrothermally prepared with an environmental friendly preparation route after pyrolysis from biomass (specifically from agricultural (potato) peels). The prepared biochars were activated with potassium hydroxide (chemical activities). The preparation route had a strong impact on the pore structure of PAC. In addition, surface chemistry was also affected by the preparation and activation process. The adsorbent materials were also characterized by Scanning Electron Microscopy. The prepared activated carbons were used as adsorbents for the removal of lead ions. Batch experiments were performed to investigate the effect of physico-chemical parameters, such as pH, contact time, initial metal concentration and temperature. Equilibrium data were analyzed using Langmuir and Freundlich isotherm models. The thermodynamic parameters such as the change of enthalpy (ΔH^0), entropy (ΔS^0) and Gibb's free energy (ΔG^0) of adsorption systems were also determined and evaluated.

Keywords: agricultural wastes; activated carbon; adsorption; lead ions; wastewaters.

1. Introduction

Recently, many researchers worldwide turned their interest to the preparation of low-cost adsorbent materials for decontamination/desalination purposes [1-4]. It is fact that these years there is a question about which adsorbent is most efficient. The first theory proposes adsorbent materials of high adsorption capacity (i.e. >200 mg/g) but with demanding synthesis steps and high cost. The other theory suggests adsorbent materials of medium adsorption capacity (50-200 mg/g) but with simple synthesis routes and really low-cost. In the latter theory, those activated carbons can be classified [5,6].

An important (but easy for reply) question is why activated carbons are such useful in adsorption technology. The activated carbons are widely used in adsorption technology due their large surface area and different surface functional groups as carboxylic, carbonylic, phenolic, quinonic, lactonic and/or other groups which are bound to the graphite-like layers [7]. For this reason, activated carbons are extensively used as optimum adsorbent materials. Numerous types of activated carbons (especially derived from fruit peels) are produced in the last years focusing on the improvement of adsorption capacity given that the cost is kept low [8-12].

In the present study, based on our previous experience/knowledge in activated carbons and low-cost adsorbent materials [4,5,13-21], activated carbons were produced from agricultural wastes by hydrothermal treatment of potato peels. All samples were activated using KOH at 400 °C. The activated carbons produced were denoted hereafter as PAC. The samples were characterized using Scanning electron microscopy (SEM) and BET analysis. The model heavy metal ions pollutant selected for the adsorption tests was lead ions (Pb(II)).

For this purpose, mainly extensive equilibrium analysis was done by fitting the equilibrium data to Langmuir and Freundlich equations. The equilibrium data were repeated similarly at 4 different temperatures (20, 30, 40, 50 °C) in order to result the respective thermodynamic evaluation of this system. Based on the fact that 4 different temperatures was examined in equilibrium, the respective thermodynamic analysis was done in order to export some very important parameters as enthalpy, entropy and free energy for the system.

2. Materials and Methods

2.1. Materials

For the preparation of activated carbons, H_3PO_4 and $\text{NiCl}_2 \cdot 6\text{H}_2\text{O}$ were obtained from Sigma-Aldrich (St. Louis, MO, USA). The potato peels used were obtained as residues/wastes after domestic (home) use.

2.2. Preparation of activated carbons by pyrolytic and hydrothermal treatment

Potato peels after being washed with distilled water to remove dust and other inorganic impurities, were dried overnight at 100 °C to reduce the moisture content. The dry material was grounded and sieved to be of uniform particle size (+0.45-0.15 mm). The final material was designated as "PP". For the hydrothermally prepared activated carbon, hydrochars were firstly prepared by hydrothermal treatment. A weighted amount of the dry potato peels precursor (20 g) was dispersed in 100 mL of water. The hydrocarbonization process (HTC) of the precursor material was carried out in a 1-L Parr stirred pressure reactor (Parr Instrument Company, Moline, Illinois). The mixture was sealed into a Teflon vessel inserted in the autoclave, which was subjected to 200 °C at a heating rate of 4 °C min⁻¹ (pressure at 200 °C of around 580 psi) with an agitation speed of 150 rpm. It was maintained at this temperature for 4 h and after this period of time the autoclave was cooled down to room temperature. The reaction mixture, was consisting of a liquid solution and a solid phase (hydrochar); the hydrochar was collected in a glass beaker for separation, was washed thoroughly with hot distilled water followed by ethanol washing and was dried at 100 °C overnight. The solid yield was determined by weight. Chemical activation of the hydrochar was performed using KOH. The impregnation ratio was calculated as the ratio of the weight of KOH in solution to the weight of the used hydrochars (the weight ratio of KOH/precursor is 1:0.9). The appropriate volume of KOH were dissolved in 250 mL of distilled water and then 20 g of the hydrochar were mixed with the KOH solution and stirred overnight in order a complete reaction between hydrochar and H_3PO_4 to be achieved. The mixture was filtered and the remaining solid was dried at 100 °C for about 24 h. It was placed then in a furnace and heated to 400 °C for 2 h at a heating rate of 25 °C/min under nitrogen flow (500 mL/min). The activated carbons formed were then treated with Soxhlet washing, freeze-drying, grounding and sieving. The yield of activated carbons was defined as the ratio of the sample weight after carbonization to the weight of the initial hydrochar.

2.4. Characterization techniques

The surface area was determined by the the BET analysis software. Surface morphologies were studied by scanning electron microscopy (SEM), performed using JEOL-JSM-6060LV Scanning Electron Microscope.

2.5. Adsorption experiments

All adsorption experiments were carried out in 3 repetitions and the average of the values was presented as experimental point in charts. At first, the effect of the pH was determined in batch

mode using fixed conditions. 0.02 g of materials (m) were added to 20 mL of adsorbate solution (V) consisted of 100 mg/L initial ion concentrations (C_0). The pH of the solution was fixed to 2, 3, 4, 5, and 6 for each flask by micro-additions of HNO_3 (0.01 mol/L) or NaOH (0.01 mol/L). The agitation rate (N) was 150 rpm using thermostatted shaking water bath (model Julabo SW-21C, Seelbach, Germany) under controlled temperature ($T = 20^\circ\text{C}$). The agitation was lasted 24 h (t). pH-effect experiments were not carried out at $\text{pH} > 6$, in order to avoid precipitation phenomena of Pb(II) . In this pH-zone, the metal ions get out of the solution due to formation of colloidal precipitate of Ni(OH)_2 and not due to the adsorption of free Pb(II) ions [22]. In general the uptake of those metals at $\text{pH} > 6$ is attributed to the formation of metal hydroxide species such as soluble Pb(OH)^+ and/or insoluble precipitate of Pb(OH)_2 . Then, after finding the optimum pH (6), the effect of the initial ion concentration was also investigated ($m = 0.02\text{ g}$, $V = 20\text{ mL}$, $T = 20^\circ\text{C}$, $N = 150\text{ rpm}$, $\text{pH} = 6$, $t = 24\text{ h}$). The initial ion concentration was ranged from 10 to 1000 mg/L. The effect of temperature in equilibrium was investigated by carrying out the same equilibrium experiments (as those of the previous paragraph), not only at 20°C but also at 30, 40, and 50°C ($m = 0.02\text{ g}$, $V = 20\text{ mL}$, $T = 20\text{--}50^\circ\text{C}$, $N = 150\text{ rpm}$, $\text{pH} = 6$, $t = 24\text{ h min}$, $C_0 = 10\text{--}1000\text{ mg/L}$). After adsorption, the Pb(II) ions were quantitatively analyzed by atomic absorption spectrometer (model Perkin-Elmer Analyst 400, Dresden, Germany) composed of FIAS 100 Flow Injection System. The removal percentage of ions after adsorption was calculated as:

$$R(\%) = \left(\frac{C_0 - C_e}{C_0} \right) \cdot 100\% \quad (1)$$

The equilibrium amount in the solid phase (Q_e , mg/g) was calculated according to the following equation:

$$Q_e = (C_0 - C_e) \cdot \left(\frac{V}{m} \right) \quad (2)$$

2.5.1. Equations (isotherm, kinetic, thermodynamic)

The experimental equilibrium data were fitted to the Langmuir (Eq. (3)) [23], Freundlich (Eq. (4)) [24], and Langmuir-Freundlich (L-F) (Eq. (5)) [24] isotherm equations expressed by the following equations:

$$Q_e = Q_{\max} \frac{K_L C_e}{1 + K_L C_e} \quad (3)$$

$$Q_e = K_F C_e^{1/n} \quad (4)$$

$$Q_e = Q_{\max} \frac{K_{LF} C_e^{1/b}}{1 + K_{LF} C_e^{1/b}} \quad (5)$$

where Q_{\max} (mg/g) is the maximum amount of adsorption; K_L (L/mg) is the Langmuir adsorption equilibrium constant; K_F ($\text{mg}^{1-1/n} \text{ L}^{1/n} \text{ g}$) is the Freundlich constant representing the adsorption capacity; n (dimensionless) is the constant depicting the adsorption intensity; K_{LF} ($\text{L/mg}^{1/b}$) is the L-F constant; b (dimensionless) is the L-F heterogeneity constant.

For the thermodynamic evaluation, three main parameters have been calculated (the change of Gibbs free energy (ΔG^0 , kJ/mol), enthalpy (ΔH^0 , kJ/mol) and entropy (ΔS^0 , kJ/mol K)) based on the isotherms resulted at 20, 30, 40, and 50°C . The system of equations below can be used for the calculation of the aforementioned thermodynamic parameters (where C_s (mg/L) is the amount adsorbed on a solid at equilibrium and R ($8.314\text{ J mol}^{-1} \text{ K}^{-1}$) is the universal gas constant) [25]:

$$K_c = \frac{C_s}{C_e} \quad (6)$$

$$\Delta G^0 = -RT \ln(K_c) \quad (7)$$

$$\Delta G^0 = \Delta H^0 - T \Delta S^0 \quad (8)$$

$$\ln(K_c) = \left(-\frac{\Delta H^0}{R} \right) \frac{1}{T} + \frac{\Delta S^0}{R} \quad (9)$$

ΔG^0 was given from Eq. (7), while ΔH^0 and ΔS^0 were given from the slop and intercept of the chart between $\ln(K_c)$ versus $1/T$ (Eq. (9)).

3. Results and Discussion

In this section, the brief characterization was discussed as well as the adsorption evaluation of the Pb(II) removal. Extensive analysis is done about the equilibrium fitting. Also, the thermodynamic evaluation gives important data about the entropy and enthalpy of the system (based on isotherms of 4 different temperatures).

3.1. Characterizations

The morphology of the prepared materials was examined by observing the respective SEM images of them (Figure 1). Many microparticles can be seen on carbons prepared. Some samples have clear holes on the surface or some of them have smooth surface. The latter can be probably due to the synthesis procedure followed [20].

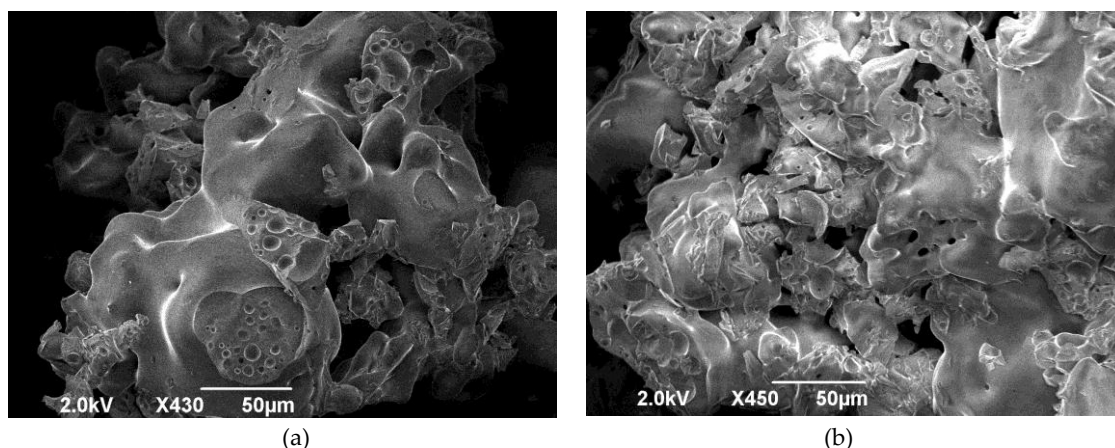


Figure 1. SEM images of the activated carbon samples prepared by hydrothermal treatment.

The activated carbons were also measured regarding their Specific Surface. The value found was 625 m²/g which can be considered as satisfactory surface area given the zero-cost first source (potato peels) and the relatively mild activation procedure.

3.2. Adsorption evaluation

3.2.1. Effect of pH

One of the most important factors which can influence the whole adsorption behavior of materials is the pH of the solution (adsorbate). So, the first factor studied in this work was the effect of pH on Pb(II) removal. Figure 2 presents the adsorption behavior of the material in 5 experimental pH values (2-6).

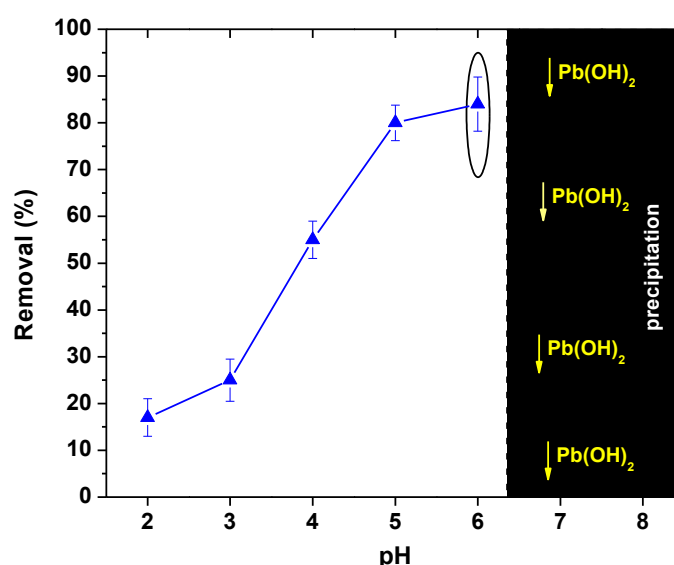


Figure 2. Effect of pH on Pb(II) adsorption by PAC.

At acidic conditions the removal of ions is lower than going to higher pH values. In particular, at pH=2, the adsorption of Pb(II) seems very low (15%). With the increase of pH values to 3, the adsorption/removal showed gradual/mild improvement (25%). The most interesting is the sharp increase at pH>3. So, at pH=4 the removal was further improved presenting the pH-curves big slopes (55%). Similar behaviour at pH=5 slopes (80%). At the final studied pH-value (6), the trend of increase was midler (84%). In general similar pH- behavior was found in other published work regarding some heavy metals removal [20,26,27], meaning low uptake at acidic and higher at neutral-alkaline conditions. As it was mentioned previously, the effect of pH was studied until pH=6, due to some possible precipitation phenomena which may be governed the whole removal process at pH>7.

3.2.2. Effect of initial Pb(II) concentration and temperature

In order to investigate the effect of initial lead ions concentration, isotherm curves was presented. According to Figure 3, the increase of initial concentration of metal caused the increase of the adsorbed amount onto solid adsorbent. The range used for the initial Pb(II) concentration was 10-1000 mg/L. For low C_0 almost the whole amount was adsorbed onto material. But, using higher concentrations ($C_0 > 300$ mg/L), the non-adsorbed amount of ions increased. This is normal due to the material's saturation.

Table 1. Equilibrium parameters for the adsorption of Pb(II) onto PAC.

Sample	T (°C)	Langmuir equation			Freundlich equation		
		Q_{max} (mg/g)	K_L (L/g)	R^2 (-)	K_F ($mg^{1-1/n} L^{1/n} g^{-1}$)	n (-)	R^2 (-)
PAC	20	217	0.01782	0.994	26.27	3.09	0.951
	30	235	0.01778	0.992	28.28	3.07	0.952
	40	236	0.01965	0.991	30.53	3.17	0.954
	50	262	0.01819	0.991	31.45	3.06	0.964

To find the maximum theoretical adsorption capacity (Q_{\max}), the equilibrium data were fitted to three isotherm models; Langmuir and Freundlich. Table 2 presents the equilibrium fitting results after running the aforementioned models. In general, the best fitting was achieved using Langmuir-equation ($R^2 = 0.991-0.994$), while Freundlich did not present good fitting results ($R^2 = 0.951-0.964$). The latter can be even visually checked by observing the curves in Figure 3.

A very interesting finding of the equilibrium data was the behavior of the hydrothermal and carbons regarding the increase of temperature (Figure 3). The increase of temperature drastically improved (21%) the Q_{\max} from 217 (20 °C) to 262 (50 °C). It is also noteworthy that the middle temperatures (30 and 40 °C) did not present significant changes (235 ad 236 mg/g).

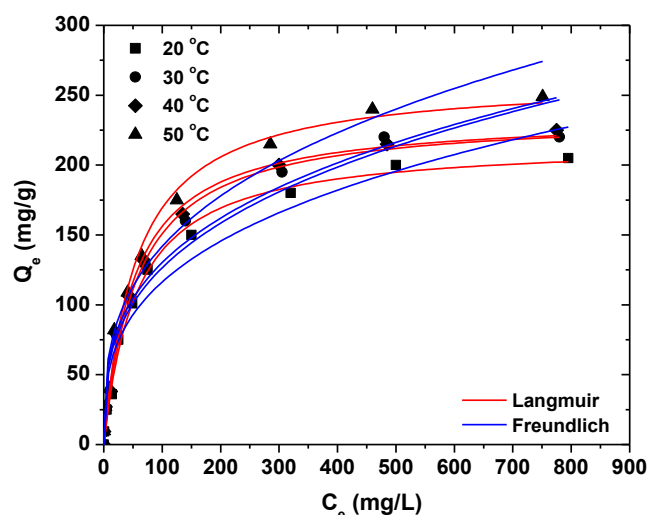


Figure 3. Effect of initial Pb(II) concentration for PAC.

In adsorption technology, it is widely known that it cannot be compared two adsorbent materials (even for the same pollutant) without keeping the same experimental conditions. Some of the basic parameters which strongly influence the whole procedure are (i) the pH solution, (ii) contact time, (iii) initial pollutant's concentration, (iv) temperature, (v) agitation speed, (vi) volume of adsorbate, (viii) ionic strength of solution, (ix) adsorbent's dosage, etc. It is clear that if any of the aforementioned conditions varies, the experiment will not be the same and consequently none comparison will be correct. Having the above in the mind, the only comparison can be realized for adsorbent/adsorbate systems of the same study.

3.2.3. Thermodynamics

One useful tool to evaluate thermodynamically the adsorbate-adsorbent system is to calculate the change of Gibbs free energy (ΔG^0 , kJ/mol), change of enthalpy (ΔH^0 , kJ/mol) and entropy change (ΔS^0 , kJ/mol K). Those thermodynamic parameters at the optimum pH found (6), at fixed initial Pb(II) concentrations (10, 100, 300, 700 mg/L) and all temperatures (20, 30, 40, 50 °C) were presented in Table 2.

ΔG^0 values were negative (for $C_0 = 10, 100, 300$ mg/L) suggesting the spontaneous adsorption of ions onto carbons. At this point, we have to take into account, that being in nature, the target is to keep or obtain the lowest energy state. So, to occur adsorption process and majorly spontaneous, the energy must be less than the initial state at the end of the process. This is the explanation why the ΔG^0 values were found to be negative. Another interesting finding is that the negatives values of ΔG^0 decreased with an increase of temperatures (from 20 to 30, and then to 40 and 50 °C). The latter may indicate the favorability of the adsorption at higher temperatures.

Table 2. Thermodynamic parameters for the adsorption of Pb(II) onto PAC.

Sample	C ₀ (mg/L)	T (K)	Q _e (mg/g)	K _c	ΔG ⁰ (kJ/mol)	ΔH ⁰ (kJ/mol)	ΔS ⁰ (kJ/mol K)
PAC	10	293	9.32	13.29	-6.30	+13.82	+0.068
		303	9.41	15.67	-6.93		
		313	9.44	15.67	-7.16		
		323	9.65	24.00	-8.54		
	100	293	75.01	3.00	-2.68	+10.79	+0.046
		303	78.23	3.55	-3.19		
		313	80.12	4.00	-3.61		
		323	82.34	4.56	-4.07		
	300	293	150.15	1.00	0.00	+8.46	+0.029
		303	161.17	1.14	-0.34		
		313	165.09	1.22	-0.52		
		323	175.81	1.40	-0.90		
	700	293	200.34	0.40	2.23	+5.99	+0.013
		303	221.31	0.46	1.97		
		313	215.62	0.44	2.12		
		323	240.24	0.52	1.75		

In the case of enthalpy, the positive values of ΔH^0 suggest the endothermicity of the process. These values were drastically diminished with the increase of C₀ (Tables 5, 6). The adsorbate ion species had to displace more than one water molecule for their adsorption and this resulted in the endothermicity of the adsorption process. So, the change of enthalpy must be positive. Another possible indication (not so crucial) about the adsorption type is the magnitude of ΔH^0 .

In the case of entropy, all values of ΔS^0 were positive. This is corresponded to the adsorbent's affinity with the adsorbate ion species. Also, when $\Delta S^0 > 0$ an increased randomness happened at the solid/solution interface. It is necessary to keep in mind that the water molecules, which were diffused into the porous network of the carbons (those which were displaced by the adsorbate lead ions), obtained big quantities of transitional entropy and in this way they allow the randomness in the system. The last point for $\Delta S^0 > 0$ is the increase in freedom degree of the bound/adsorbed ions [28].

At this point it is mandatory to say some few words about the reuse potential of activated carbons. In general, the exothermic nature of the adsorption is used in the heat treatment process and leads to desorption, partial cracking and polymerization of the organics adsorbed. The removal of charred organic residue formed in the porous structures is conducted in the final stage. The porous carbon structure regenerating its original surface characteristics will be revealed in this manner. The adsorption columns can be reused after treatment. Generally, the adsorptive capacity is reduced after the burning of the pre-adsorption thermal regeneration cycle between 5-15 wt% of the carbon bed [29]. High temperatures are required in the process of thermal regeneration, which means that the energies involved in this process are high. This process is hence energetically and commercially expensive [30]. Before it is feasible to have regeneration facilities on site, a certain size has to be attained for the plants based on thermal regeneration of activated carbon. Smaller waste treatment sites normally transport their activated carbon cores to specialized facilities for regeneration. This increases the footprint of the carbon [31].

3.3. Cost-effectiveness of agricultural-based activated carbons

To better understand the value of the activated carbon from agricultural wastes (not especially from potato), a scenario with many hypotheses is set-up. The basic parameters hypothetically are the same apart from the maximum theoretical adsorption capacity (Q_{\max}) and the estimated cost for the adsorbent production. In that case, 5, and 3.3 kg of AC and ACM required for decontamination. If the cost production for an agricultural waste is zero, then the production of AC is expected to be

at least 4 times larger (electricity for pyrolysis etc), while the respective for ACM 6 times larger (pyrolysis, chemical modification etc). It is clear that the order of profitability using the above adsorbents will be $AC > ACM$.

In order to make a more realistic scenario, for an average industry which treats and discharges 1 MGD (megagallons per day) as effluents (containing either dyes or metals), the approximate quantity of adsorbents can be calculated. In the case of textile industries, dye concentrations of 0.01-0.25 g/dm³ (= 10-250 g of dye per m³ of effluent) have been cited as being present in dyehouse effluents, depending on the dyes and processes used [32]. Therefore, 37.85-946.25 kg of dye (containing into the dyeing effluent) per day must be removed/adsorbed. Having as basis the example of Table 7, 189-4731 kg of AC and 126-3154 kg of ACM are needed for the efficient treatment of effluent. The same example for an average metal plating (chromium) with 2 MGD as effluent rate can be calculated mentioning that chromium concentrations of 0.5-270,000 g per m³ of effluent have been cited [33].

4. Conclusions

This paper investigates the synthesis of activated carbons with hydrothermal treatment using potato peels as source. The activation was done with KOH at 400 °C. The pH-effect experiments confirmed lower ion removal at acidic conditions, while going to higher pH values the removal increased (pH optimum was 6). The increase of temperature drastically improved (21%) the Q_{\max} of PAC from 217 (20 °C) to 262 (50 °C). From SEM images, many microparticles can be seen and some of them have clear holes on the surface.

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